

CWS - Potential Energy

①

The work energy theorem related the change in Kinetic Energy to the Work done on/by the system,

$$\Delta K_{\text{sys}} = W.$$

We found that the Work done by any force is given by,

$$W = \int_C \vec{F} \cdot d\vec{r}$$

where C is the particular path taken

For a particular kind of force that integral is path independent.

Conservative Forces

(2)

There are a number of ways to define a conservative force, each can be derived from the other.

(i) $\nabla \times \vec{F} = 0$ \Leftarrow only $\vec{F}(\vec{r})$
no $\vec{F}(\dot{\vec{r}})$

(ii) $\oint_C \vec{F} \cdot d\vec{r} = 0$ \Leftarrow no energy change around any closed loop.

(iii) $\int_C \vec{F} \cdot d\vec{r}$ is path independent
 \Leftarrow the integral depends only on the end pts.

These properties suggest we define a quantity dependent on location whose difference is proportional to the work integral

Define Potential Energy

(3)

$$\Delta PE = U(\vec{r}_f) - U(\vec{r}_i) = \Delta U = - \int_{\vec{r}_i}^{\vec{r}_f} \vec{F}(\vec{r}) \cdot d\vec{r}$$

In 1D,

$$\Delta U_{\text{sys}} = - \int_{x_A}^{x_B} F(x) dx$$

The prior properties and the above definition give the following relationship

$$\vec{F}(\vec{r}) = -\nabla U(\vec{r})$$

where

$$\nabla = \hat{x} \frac{d}{dx} + \hat{y} \frac{d}{dy} + \hat{z} \frac{d}{dz}$$

- One core definition of a conservative force guarantees that an appropriately

defined potential, $U(x)$, leads to a conservative force.

(4)

$$\vec{F}(\vec{r}) = -\nabla U(\vec{r})$$

$$\nabla \times \vec{F} = \nabla \times (-\nabla U) = -\nabla \times \nabla U = 0$$

$$\nabla \times \nabla f(\vec{r}) = 0$$

the curl of
a gradient is
zero

Proof:

$$\nabla f(\vec{r}) = \left\langle \frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z} \right\rangle$$

$$\nabla \times \nabla f = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \frac{\partial f}{\partial x} & \frac{\partial f}{\partial y} & \frac{\partial f}{\partial z} \end{vmatrix}$$

let's focus on $(\nabla \times \nabla f)_x$,

(5)

$$(\nabla \times \nabla f)_x = \frac{\partial}{\partial y} \left(\frac{\partial f}{\partial z} \right) - \frac{\partial}{\partial z} \left(\frac{\partial f}{\partial y} \right)$$

$$= \frac{\partial^2 f}{\partial y \partial z} - \frac{\partial^2 f}{\partial z \partial y}$$

partial
derivative
operator is
linear so,

$$\frac{\partial^2 f}{\partial y \partial z} = \frac{\partial^2 f}{\partial z \partial y}$$

= 0

true for every component

$$\nabla \times \nabla f(\vec{r}) = 0$$

Returning to the work-energy theorem

$$\Delta K_{\text{sys}} = W = \int_C \vec{F} \cdot d\vec{r}$$

conservative
force?

$$\Delta K_{\text{sys}} - \int_C \vec{F} \cdot d\vec{r} = 0$$

$$\Delta K_{\text{sys}} + \Delta U_{\text{sys}} = 0$$

kinetic
potential
energy eqn.

⑥

Common Forms of Writing this ↗

$$\Delta KE + \Delta PE = 0$$

$$\Delta K + \Delta U = 0$$

$$\Delta T + \Delta U = 0$$

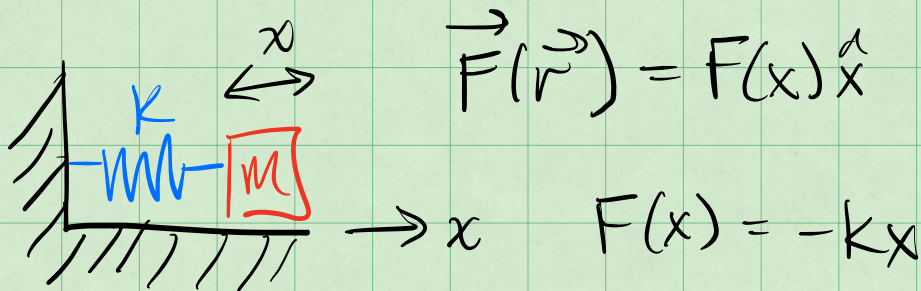
$$\Delta T + \Delta V = 0$$

most common
and the form
we will use in
class.

Now what?

Let's explore some examples and investigate the potential landscape, the type of motion we expect, stability/instability, and classical turning points.

Example: Simple Harmonic Oscillator (7)



$$U(x) = -\int_0^x F(x') dx' = \frac{1}{2} kx^2$$

The SHO is a conservative system so that,

$$\Delta K + \Delta U = 0$$

or,

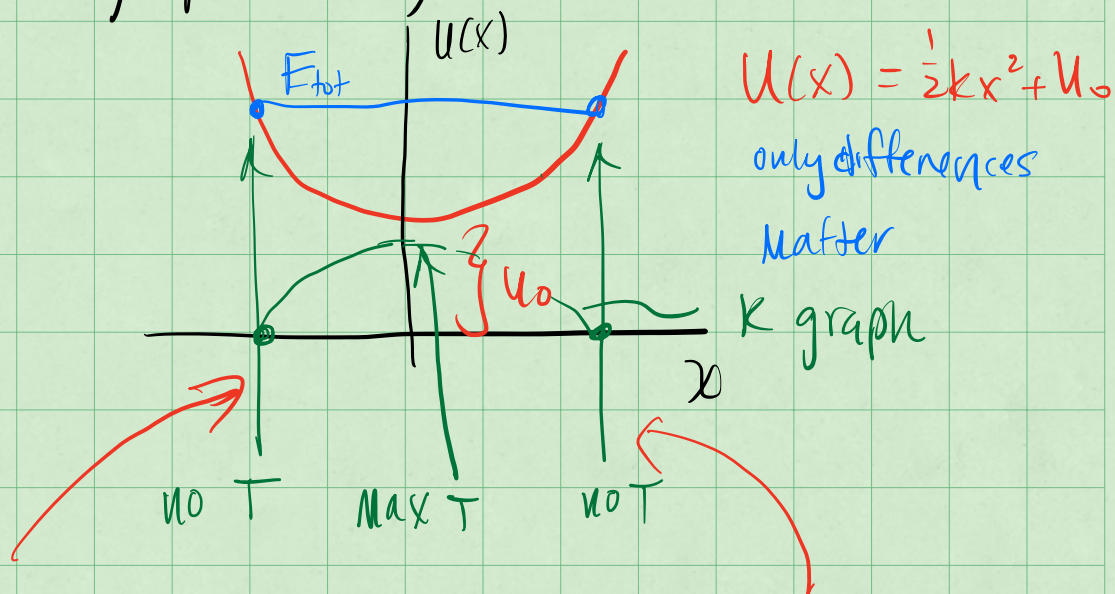
$$K + U = E_{\text{tot}} = \underline{\text{constant}}$$

This means we can analyze the motion of the system by assuming a total amount of available energy.

$$K(v) + U(x) = E_{\text{tot}} \Rightarrow \underline{v(x) \text{ or } x(v)} @ E_{\text{tot}}$$

We can find phase trajectories of the motion at a given total energy, E_{tot} . 8

Let's graph $U(x)$,



No motion beyond here; classical turning points
this shows that the SHO turns around at those
maximum values for x . We also note
the $\text{MAX } T$ (max speed) is at $x=0$,
where $\text{min } U$ occurs.

This motion is stable about $x=0$.

why?

Stability

(9)

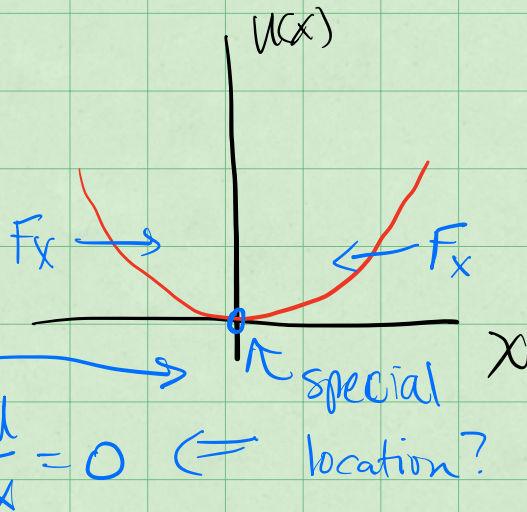
lets use the SHO example

$$U(x) = \frac{1}{2}kx^2$$

$$F(x) = -\frac{dU}{dx}$$

$$F(x) = -kx$$

forces push mass
towards $x=0$



$$\frac{dU}{dx} = 0 \quad \leftarrow \text{special location?}$$

Finding critical points

$x=0$ for $U = \frac{1}{2}kx^2$ is a "critical point" a point where

$F_x = 0$. We can find those points, x^* , by taking the first

derivative of the potential and solving the resulting equation.

$$U = \frac{1}{2}kx^2 \quad \frac{dU(x^*)}{dx} = 0 \quad \text{solve for } x^* \quad (10)$$

$$\frac{dU(x^*)}{dx} = kx^* = 0 \quad x^* = 0 \quad \text{as predicted before}$$

How do we see the fact that this point is stable?

→ we use the second derivative (curvature of $U(x)$) at x^*

$$\frac{d^2U(x^*)}{dx^2} = k > 0$$

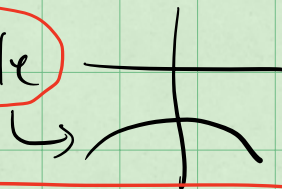
this is the condition for stability

upward facing curvature



so,

$$\frac{d^2U(x^*)}{dx^2} < 0 \quad \text{unstable}$$



finally,

$$\frac{d^2U(x^*)}{dx^2} = 0 \Rightarrow \text{flat (metastable)}$$

Summary for 1D potentials

(11)

- With $U(x)$, $F(x) = -dU/dx$
- Find critical points, x^* , using the first derivative.

$$\frac{dU(x^*)}{dx} = 0$$

solve for x^*

↓
critical points

- With x^* , we can find stability,

$$\frac{d^2U(x^*)}{dx^2} > 0$$

stable

$$\frac{d^2U(x^*)}{dx^2} < 0$$

unstable

$$\frac{d^2U(x^*)}{dx^2} = 0$$

meta stable

Example: Morse Potential

(12)

The Morse potential is a model of diatomic atoms. It's a toy model and we will explore it in one dimension,

$$U(x) = D_e \left(1 - e^{-\alpha(x-x_e)} \right)^2$$

Here we have a modified spring with constant, k_e . The remaining coefficients are,

D_e : well depth

x_e : equilibrium bond length

$\alpha = \sqrt{k_e/2D_e}$: parameter representing the spring & well depth

With $U(x) = D_e \left(1 - e^{-\alpha(x-x_e)}\right)^2$ (13)

$$F(x) = -\frac{dU}{dx}$$

$$= -\frac{d}{dx} \left(D_e \left(1 - e^{-\alpha(x-x_e)}\right)^2 \right)$$

$$= -2D_e \left(1 - e^{-\alpha(x-x_e)}\right) \left(\alpha e^{-\alpha(x-x_e)} \right)$$

$$F(x) = -2D_e \alpha \left(1 - e^{-\alpha(x-x_e)}\right) e^{-\alpha(x-x_e)}$$

$\nabla_x \vec{F} = 0$? \star conservative force

$\vec{F}(\vec{r}) = F(x) \hat{x} \rightarrow \nabla_x \vec{F}$?

\hat{x} component get $\frac{dF_x}{dy} \downarrow \frac{dF_x}{dz}$

Both are zero \nearrow $\xrightarrow{\text{b/c}}$ $F_x(x)$

Stability? what is x^* ?

(14)

$$\frac{dU(x^*)}{dx} = 0$$

$$\frac{dU(x^*)}{dx} = 2De^{\alpha} (1 - e^{-\alpha(x^* - x_e)}) e^{-\alpha(x^* - x_e)}$$
$$= 0$$

Both terms could vanish,

$$e^{-\alpha(x^* - x_e)} = 0 \quad (1)$$

$$(1 - e^{-\alpha(x^* - x_e)}) = 0 \quad (2)$$

For eqn 1,

$$\lim_{x^* \rightarrow \infty} e^{-\alpha(x^* - x_e)} = 0 \quad \boxed{x^* \rightarrow \infty}$$

For eqn 2,

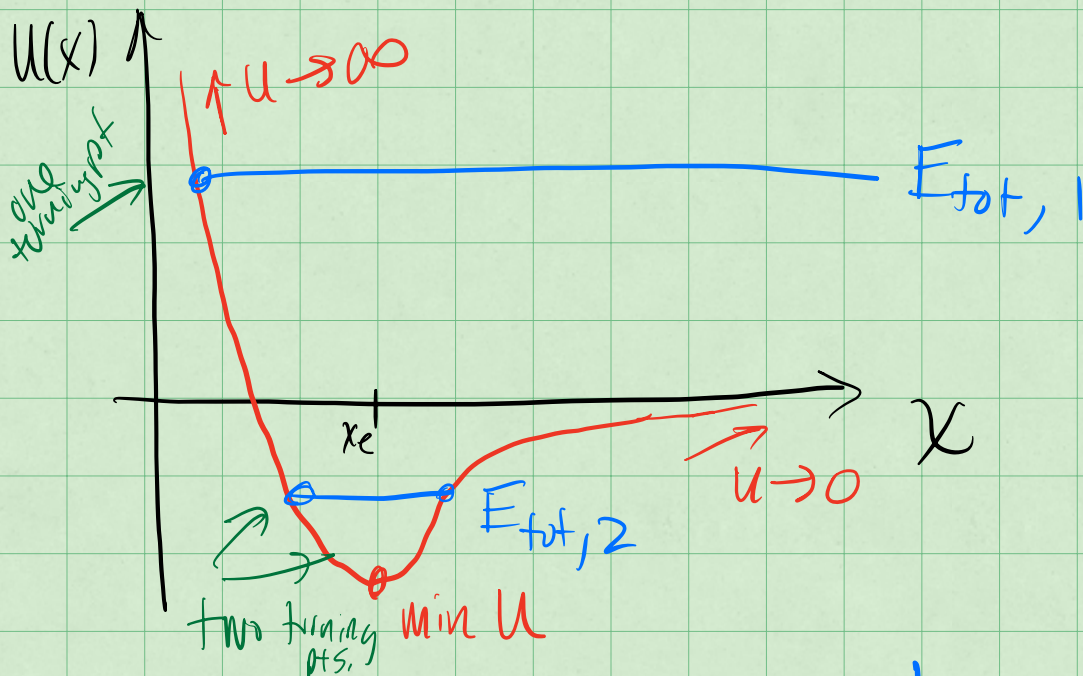
(15)

$$(1 - e^{-\alpha(x^* - x_e)}) = 0$$

$$-\alpha(x^* - x_e) = \ln(1) = 0$$

$$x^* = x_e$$

Two critical points. Why?



2 different kinds of motion!

$x^* = x_e$ looks stable, is it?

16

$$\frac{d^2 U(x_e)}{dx^2} = ?$$

$$\frac{dU(x)}{dx} = 2D_e \alpha (1 - e^{-\alpha(x-x_e)}) e^{-\alpha(x-x_e)}$$

$$\frac{d^2 U(x_e)}{dx^2} = 2D_e \alpha \left\{ \begin{aligned} & \left(\alpha e^{-\alpha(x-x_e)} \right) e^{-\alpha(x-x_e)} \\ & + (1 - e^{-\alpha(x-x_e)}) (-\alpha e^{-\alpha(x-x_e)}) \end{aligned} \right\}$$

$$= 2D_e \alpha (\alpha + (1-1)(-\alpha)) = 2D_e \alpha^2 > 0$$

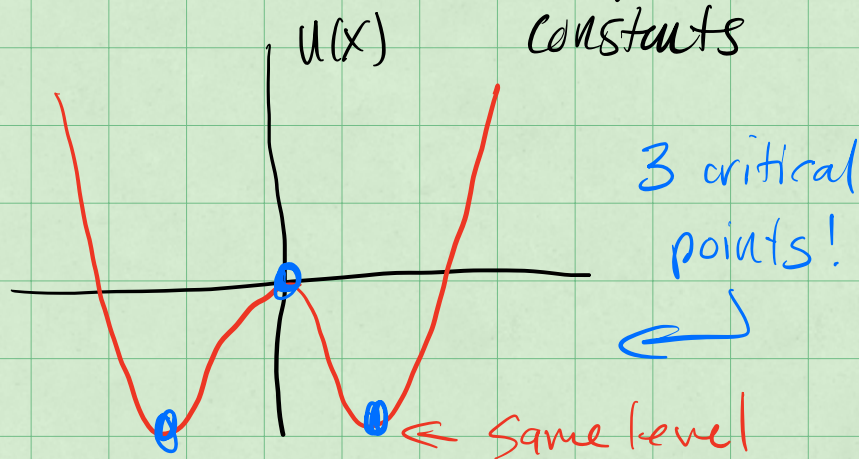
stable critical point, $x^* = x_e$

Example: Double Well Potential

(17)

$$U(x) = ax^4 - bx^2 \quad \text{where } a \neq b$$

$a, b > 0$ ← are positive constants



$$U(x) = ax^4 - bx^2$$

$$F(x) = -\frac{dU}{dx} = -4ax^3 + 2bx$$

What about these critical points, x^* ?

$$\frac{dU(x^*)}{dx} = 0 \quad \& \text{ solve}$$

$$\frac{dU(x^*)}{dx} = 4ax^{*3} - 2bx^* = 0$$

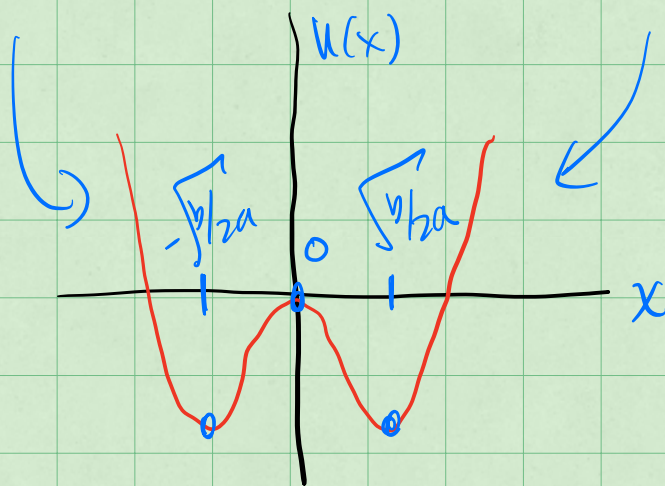
(10)

$$x^*(4ax^{*2} - 2b) = 0$$



$$x^* = 0$$

$$x^* = \pm \sqrt{\frac{b}{2a}}$$



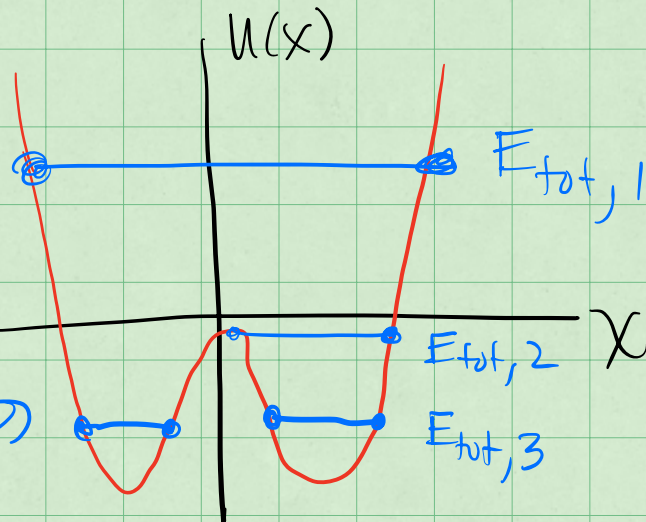
Stability? let's just look at $x^* = 0$

$$\begin{aligned} \frac{d^2U(x^*)}{dx^2} &= 12ax^{*2} - 2b \\ &= -2b < 0 \end{aligned}$$

unstable!

(19)

Different motion and turning pts based of E_{tot}



Trajectories? $v(x)$; $x(v)$?

Pick an E_{tot} ,

$$T + U = E_{tot} = \text{constant}$$

$$\frac{1}{2} m v_x^2 + (a x^4 - b x^2) = E_{tot}$$

$$v_x(x) = \pm \sqrt{\frac{2(E_{tot} - a x^4 + b x^2)}{m}}$$

this puts a limit of the total

energy for this model to make sense,

20

$V_x(x)$ must be real so,

$$E_{tot} - ax^4 + bx^2 \geq 0$$

$$E_{tot} \geq -bx^2 + ax^4$$

The location where $U(x)$ is smallest is

$$x^* = \pm \sqrt{b/2a}$$

$$E_{tot} \geq -b\left(\frac{b}{2a}\right) + a\left(\frac{b}{2a}\right)^2$$

$$\geq \frac{-b^2}{2a} + \frac{b^2}{4a} = \frac{-b^2}{4a}$$

$$E_{tot} \geq \frac{-b^2}{4a} \quad \text{for given } a \text{ and } b$$